

Anomalous Temperature Dependence of the Heat of Hydration of Natrolite

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Abstract: The temperature dependence of the heat of hydration of natrolite was studied by isothermal adsorption calorimetry from 412 to 472 K. The heat capacity of hydration implied by these results is about 5 times greater than the calorimetric heat capacity of reaction, suggesting atypical behavior across this solid solution.

Key Words: Natrolite, hydration, differential scanning calorimetry, enthalpy.

1. INTRODUCTION

Natrolite is a natural zeolite with an essentially stoichiometric composition ($\text{Na}_2\text{Al}_2\text{Si}_3\text{O}_{10}\cdot 2\text{H}_2\text{O}$; [1]). Its crystal structure is well-known, including positions of H_2O molecules (in fact, it was the first zeolite structure refined; [1-5]). The framework of natrolite is composed of Si- and Al-centered tetrahedra. The arrangement of Si and Al in the tetrahedral sites is variable but tends to be largely ordered [6, 7]. Channels within the structure contain two Na^+ ions and two H_2O molecules per ten framework oxygens oriented in zigzag chains with each Na^+ coordinated to four framework oxygens and two H_2O molecules [3, 8, 9].

The importance of natrolite as a rock-forming mineral [e.g., 1, 7] and its regular compositional and structural properties have led many workers to use this mineral as a reference for studying zeolite dehydration reactions [9-13]. However, unlike most zeolite dehydration reactions that proceed in a continuous fashion with increasing temperature, implying complete solution between the hydrated forms [e.g. 1, 13-16], the dehydration of natrolite occurs abruptly as a function of temperature, as indicated by both isothermal, equilibrium measurements [10] and scanning heating thermogravimetric analysis (TGA; Fig. 1) [see also 1, 13] indicate that dehydration of natrolite occurs abruptly as a function of temperature. This can be seen in the TGA curve of Fig. (1), where it can be seen that the mass of natrolite initially decreases gradually with temperature between 400 and 550 K and then decreases dramatically at ~ 575 K. In contrast to the sharp "right angle" topology of the TGA curve of Fig. (1) at 600 K, most zeolites exhibit a more gradual, curved topology in TGA signals as complete dehydration is reached. In addition, a pronounced hysteresis is observed in TGA studies of dehydration/rehydration of natrolite under constant water vapor pressure ($P_{\text{H}_2\text{O}}$) with rehydration occurring at significantly lower temperatures [13] in contrast to the behavior of many zeolites. The cause(s) of these phenomena are not known, in part because little data are avail-

able for evaluating the thermodynamic properties of natrolite dehydration.

The present study investigates the thermodynamic behavior of the natrolite- H_2O system through isothermal adsorption heat measurements as a function of temperature. Reaction behavior exhibited in these experiments indicates that a solvus exists between natrolite and dehydrated natrolite. For the first time, the temperature dependence of the heat of hydration has been directly determined and compared to that calculated from the heat capacities of hydrated and dehydrated natrolite and water vapor. These results demonstrate excess heat capacity across the natrolite-dehydrated natrolite solid solution. Combined, the observations of this study provide evidence for a solvus in the natrolite-dehydrated natrolite solid solution that explains many of the anomalous thermal analysis behaviors exhibited by this mineral.

2. MATERIALS AND METHODOLOGY

The sample of natrolite was previously described and characterized by Neuhoff *et al.* [7; sample NAT001]. It was collected as veins within a metabasaltic tectonic inclusion at the famous Dallas Gem Mine benitoite and neptunite locality, San Benito County, California. Phase pure separates were hand picked, ground in an agate mortar, and sieved to a 20-40 μm size fraction. Sample identification and purity were confirmed by X-ray powder diffraction. The composition was determined by electron probe microanalysis at Stanford University to be essentially stoichiometric ($\text{Na}_2\text{Al}_2\text{Si}_3\text{O}_{10}\cdot n\text{H}_2\text{O}$). Water content of the sample was determined in this study by thermogravimetric heating to 1023 K after the equilibration with a room temperature atmosphere of 50 % relative humidity. The mass loss is about 9.49% of total sample mass, very close to the ideal water content of natrolite (9.48%), and the water content taken to be 2 moles of water per formula unit.

All the experiments in this study were conducted on the Netzsch STA 449C Jupiter simultaneous thermal analysis system at the University of Florida. The core component of the system is a vacuum-tight liquid nitrogen cooled furnace enclosing a sample carrier with an electrode for measurement of temperature differences between the sample and a

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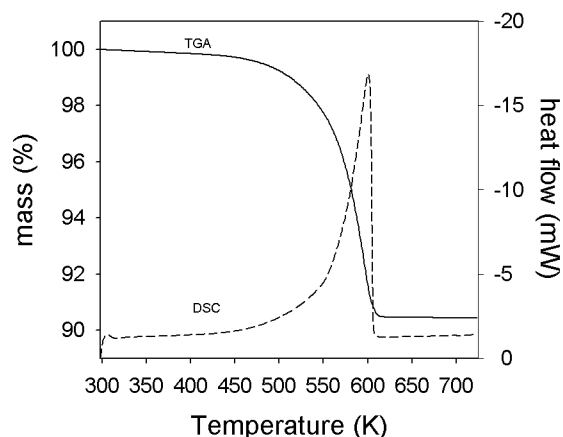


Fig. (1). Scanning-heating (2K/min) TGA (solid) and differential scanning calorimetric (DSC; dashed) behavior of natrolite. Note the abrupt mass loss between 550 and 600 K accompanied by sharp peak in the DSC signal.

reference pan, generating a heat flux differential scanning calorimetric (DSC) signal. With respect to the present study, an essential aspect of this setup is that the DSC signal is measured simultaneously with TGA signals from a microbalance connected to the sample carrier. This allows the DSC signal to be interpreted directly in terms of water loss or gain to the sample as measured by TGA. All experiments were performed under ultrapure dry or humidified N_2 gas.

Temperature and caloric calibrations were performed using data based on the DSC response of standard materials. A multipoint temperature calibration curve was developed using the melting points of H_2O , Ga, In, Sn, Bi, Zn and Al along with the solid-solid transition points of CsCl and quartz [17-20]. Because many of these materials are incompatible with the Pt-Rh crucible used in the experiments, temperature calibration was conducted in identical crucibles lined with a sub-mm thick insert of alumina. Caloric calibration was accomplished by the heat-flow rate method [18] using the DSC response of synthetic sapphire [18-22]. The background-corrected DSC response of a synthetic sapphire disc similar in mass to the experimental charges was measured at heating rates of 5, 10, 15 and 20 K/min over the range of temperatures encountered in this study. Caloric calibration factors calculated from results at each heating rate agreed within 1% and were a nearly linear function of temperature.

The hydration behavior and heats of hydration of natrolite were assessed under isothermal conditions through isothermal DSC measurements [23]. In each experiment, 20 to 30 mg of hydrated natrolite was placed into an unsealed Pt-Rh crucible with perforated lid and dehydrated by scanning heating from 298 to 733 K at the rate of 15 K/min. Care was taken to avoid heating the sample to temperatures under which dehydrated natrolite ("metanatlolite") transforms irreversibly to the form known as β -metanatlolite [11, 24]. The sample was then allowed to cool to the experimental temperature under dry N_2 gas. After equilibration (20-40 min) under dry gas at this temperature until both DSC and TGA

baselines stabilized, the gas stream was changed to humid N_2 which was generated by bubbling N_2 through saturated NaCl solution (resulting in an experimental P_{H_2O} of ~ 12 mbar; P_{H_2O} was monitored continuously on the gas stream exiting the system using a flow-through humidity meter manufactured by Sable Systems). The sample was allowed to react until the DSC and TGA baselines stabilized again, indicating a cessation of reaction. Repeated experiments on the same sample indicated a progressive loss of hydration capacity coupled with progressively less energetic heats of reaction. Consequently, a fresh aliquot of sample was used for each experiment.

3. ISOTHERMAL HYDRATION BEHAVIOR OF NATROLITE

Figs. (2 and 3) illustrate the results of isothermal hydration experiments on natrolite at 382 and 482 K, respectively. The shaded areas of the figures represent isothermal equilibrium of anhydrous natrolite under a flow of dry N_2 gas, which was followed by introduction of humidified N_2 resulting in uptake of H_2O by natrolite shortly after the gas composition changed. The hydration of natrolite in both experiments is manifested by the abrupt increase in sample mass accompanied by an endothermic deflection in the DSC signal. The rate of rehydration, given by the first derivative of the TGA signal (DTG) is similar in form to the DSC signal, suggesting little overall change in the average enthalpy of reaction over the course of hydration.

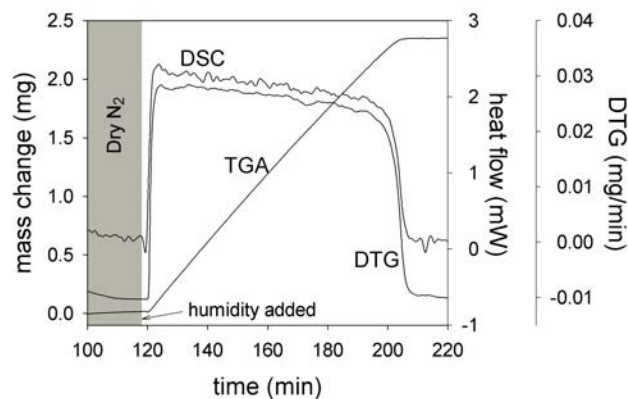


Fig. (2). Example immersion experiment on natrolite conducted at 382 K. Region of the figure encompassed by the gray box denotes initial equilibration of sample at experimental temperature under dry N_2 . The rest of the experiment was conducted in the presence of a flow of humidified N_2 .

Close inspection of the TGA data in Figs. (2 and 3) indicates that the rate of hydration differs between the beginning, middle (majority) and end of the reaction. Initial reaction involves a rapid increase in the rate of hydration (denoted by the positive deflection in the DTG signal). After this initial stage, the rate of hydration is relatively constant for the majority of reaction (near-zero order) until the final portion of the reaction, where the rate of reaction decreases exponentially. The duration of these stages varies with temperature. It can be seen in Fig. (2) that essentially the whole course of reaction at 382 K is characterized by near-zero order rate behavior (except for rapid increases and decreases in reac-

tion rate at the induction and cessation of reaction, respectively). At 482 K (Fig. 3) the zero order portion of the reaction only lasts through about half of the reaction, being followed by a segment where the reaction rate decreases exponentially until reaction stops. It is shown below that these reaction behaviors change progressively between these temperatures.

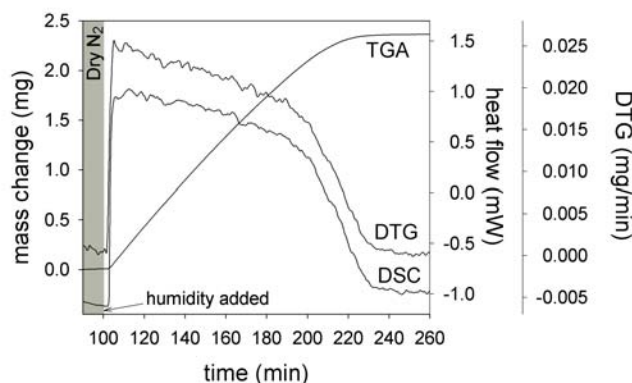


Fig. (3). Example immersion experiment on natrolite conducted at 482 K. See caption to Fig. 2 for explanation.

The dependence of reaction rate on degree of reaction in natrolite is markedly different from that found in other zeolite hydration and dehydration reactions which typically exhibit an exponential decrease in rate as the reaction progresses [14, 23, 25]. This behavior is only apparent in the last half of the experiment shown in Fig. (3). The abrupt increases in rate at the beginning and decreases in rate at the end of the experiments shown in Figs. (2 and 3) are probably artifacts of the induction and cessation of reaction, respectively. The curious aspect of these experiments is the near-zero order reaction kinetics that dominates reaction behavior at 382 K and occurs over about the first half of the reaction at 482 K. This behavior has been noted previously [23, 26] both during hydration and dehydration reactions in natrolite although its temperature dependence has not been previously studied in detail.

Fig. (4) shows the rate behavior of rehydration in natrolite at several different temperatures as a function of the degree of rehydration (cast in terms of the mole fraction of hydrated natrolite, $X_{\text{hydrated natrolite}}$). In all cases, the DSC signals (not shown) were topologically similar to the DTG signals as in Figs. (2 and 3). Comparison of the results in Fig. (4) indicates several trends with increasing temperature. First, the degree of hydration obtained under the experimental conditions (~ 13 mbar $P_{\text{H}_2\text{O}}$) decreases progressively with increasing temperature reflecting the tendency of the mineral to progressively dehydrate with increasing temperature. Second, the apparent rate of hydration decreases with increasing temperature (as indicated by the decreasing DTG values with increased temperature for a given value of $X_{\text{hydrated natrolite}}$). This effect appears counter to the typical increase in reaction rates with increasing temperature. The cause of this phenomenon is unclear, but may be related to the lower degree of hydration possible with increasing temperature (and thus lowering the thermodynamic driving force). The third phenomenon apparent in Fig. (4) is that the compositional extent of the zero-order kinetic behavior decreases with increasing

temperature. At 412 K, this behavior is observed over essentially the whole range of natrolite composition, whereas it is present only up to $X_{\text{hydrated natrolite}} = \sim 0.6$ at 472 K. The potential causes of this phenomenon are discussed below.

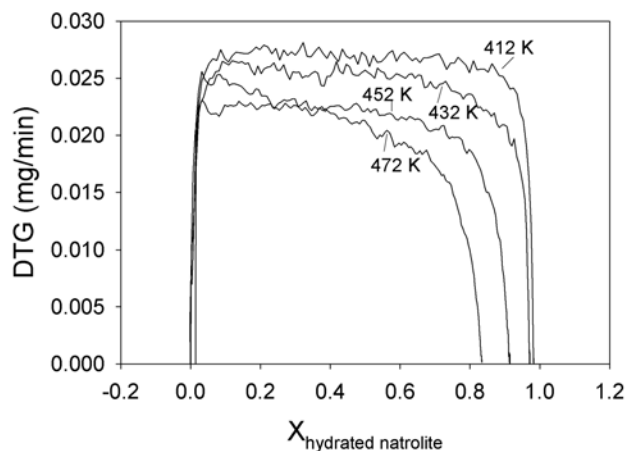


Fig. (4). Comparison between the rate of hydration in natrolite as a function of temperature and degree of hydration.

4. TEMPERATURE DEPENDENCE OF THE HYDRATION HEAT OF NATROLITE

The heat flow during hydration of natrolite is proportional to the area under the DSC curve, which allows a calculation of the enthalpy of hydration (ΔH_{hyd}) by the equation:

$$\Delta H_{\text{hyd}} = -18.015 A / k m_{\text{gain}} \quad (1)$$

where A is the area under the DSC curve, m_{gain} is the mass gain in the rehydration and k is the caloric calibration factor. The results of ΔH_{hyd} for natrolite at four temperatures for which multiple experiments were conducted are listed in Table 1 and shown in Fig. (5) (the experiments shown above at 382 K and 482 K were of insufficient quality to derive useful heat values). The values of ΔH_{hyd} at the same temperature are very close ($<0.5\%$ difference), and the reported

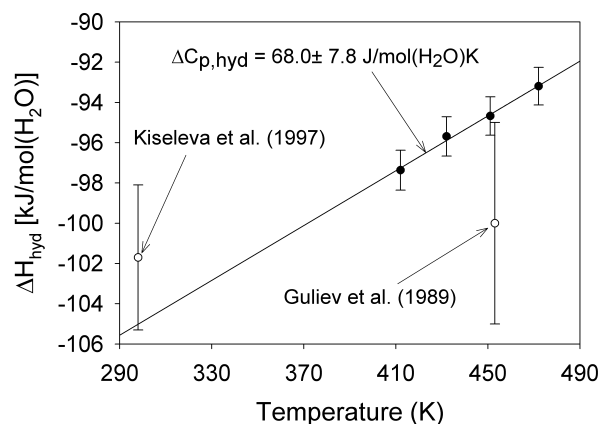


Fig. (5). Enthalpy of hydration of natrolite as a function of temperature. Solid symbols show data generated in this study, open symbols refer to previously reported values [24, 25]. Linear regression of data generated in this study is shown by solid line; slope of this regression corresponds to $\Delta C_{p,\text{hyd}}$.

Table 1. Isothermal Immersion Calorimetric Data for Natrolite

T (K)	Sample Mass (mg)	Duration ¹ (min)	Mass Gain ² (%)	ΔH_{hyd} (kJ/mol-H ₂ O)	$\Delta H_{\text{hyd, ave}}$ ³ (kJ/mol-H ₂ O)	Error (kJ/mol-H ₂ O)
412	23.97	121	9.18	-97.16	-97.37	0.99
412	25.41	100	9.17	-97.50		
412	25.48	95	9.34	-97.44		
432	24.4	87	9.18	-95.74	-95.69	0.97
432	24.24	83	9.24	-95.49		
432	29.76	117	9.21	-95.84		
451	29.44	127	9.17	-94.70	-94.67	0.95
451	23.6	114	9.15	-94.55		
451	27.56	109	9.14	-94.77		
472	29.34	130	8.96	-93.21	-93.19	0.93
472	27.45	126	8.93	-93.21		
472	25.73	118	8.94	-93.16		

¹Duration of immersion portion of experiment used in data regression.

²Mass of the H₂O (in percentage) absorbed in that period.

³The average value of ΔH_{hyd} , as the integral enthalpy of hydration in natrolite.

errors include contributions from both the data variance at a given temperature and the error in the calorimetric calibration (~ 1.5%). The data indicate that ΔH_{hyd} becomes significantly less energetic with increasing temperature, increasing from ~ -97.4 kJ/mol(H₂O) at 412 K to ~ -93.2 kJ/mol(H₂O) at 472 K.

The results shown in Table 1 and Fig. (5) are generally consistent with those reported previous in the literature (Table 2). Our determination of ΔH_{hyd} at 451 K in Table 1 is less energetic than, but within error of, the previous determination by immersion calorimetry at a similar temperature [25]. The other values of ΔH_{hyd} for natrolite reported in the literature were determined at significantly different temperatures; however, all of the data are similar in magnitude to (and mostly within error of) the results from this study. Of particular note is the value determined at 298.15 K by [24] using transposed temperature drop calorimetry, which appears

to lie along trend with the data generated in this study if reported errors are taken into account.

The temperature dependence of the data shown in Fig. (5) corresponds to the heat capacity of hydration ($\Delta C_{\text{p,hyd}}$) via the relation

$$\left(\frac{\partial \Delta H_{\text{hyd}}}{\partial T} \right) = \Delta C_{\text{p,hyd}} \quad (2)$$

The linear regression shown in Fig. (5) thus corresponds to the average value of $\Delta C_{\text{p,hyd}}$ over the temperature interval of the ΔH_{hyd} data (note that previously reported values were not included in the regression). It can be seen from Fig. (5) that the results of this regression calculation are consistent with ΔH_{hyd} reported by [24] at 298.15 K. The value of $\Delta C_{\text{p,hyd}}$ determined from this regression, $68.0 \pm 7.8 \text{ J/mol(H}_2\text{O)K}$, is anomalously large relative to previously determined values

Table 2. Enthalpy of Hydration in Natrolite

Composition	Method ¹ and Reference	Temperature (K)	ΔH_{hyd} (kJ/mol-H ₂ O)
(NaAl) ₂ Si ₂ O ₁₀ ·2H ₂ O	TTD, [24]	298.15	-101.7 ± 3.6
(NaAl) ₂ Si ₂ O ₁₀ ·2H ₂ O	PE, [10]	900	-108
Not reported	PE, [12]	684.15	-102.9 ± 4.0
Not reported	DSC, [13]	623.15	-89.1
(NaAl) ₂ Si ₂ O ₁₀ ·2H ₂ O	IM, [25]	453.15	-100.0 ± 5.0

¹Methods: TTD: transposed temperature drop calorimetry; PE: retrieval from phase equilibrium observations; DSC: calculated from scanning DSC measurement; IM: heat of immersion in water.

for natrolite or other zeolites. The same sample used in this study was used to determine $\Delta C_{p,\text{hyd}}$ previously by DSC measurement of the heat capacities (C_p) of homologous hydrated and dehydrated natrolite [26]. At the lower end of the data shown in Fig. (5), $\Delta C_{p,\text{hyd}}$ was found by [26] to be ~ 17 kJ/mol(H₂O). Partial dehydration of the sample precluded determination of C_p of hydrated natrolite above ~ 403 K by [26]. However, using C_p data generated by [27] for natrolite and those of [26] for dehydrated natrolite indicate that $\Delta C_{p,\text{hyd}}$ at 472 K (the highest temperature datapoint in Fig. (5)) is essentially the same as that found at 403 K. Thus, $\Delta C_{p,\text{hyd}}$ determined by direct determination of C_p for hydrated and dehydrated natrolite is lower than suggested by the regression in Fig. (5) by a factor of ~ 4 . Another indication of the anomalous value of $\Delta C_{p,\text{hyd}}$ given by the regression in Fig. (5) is the fact that in other zeolites, $\Delta C_{p,\text{hyd}}$ rarely exceeds ~ 25 J/mol(H₂O)K [26, 28]. This is consistent with statistical mechanical models of the heat capacities of confined water molecules in zeolites, which suggest that $\Delta C_{p,\text{hyd}}$ should not exceed $3R$ (where R is the gas constant) [28, 29]. Thus, the temperature dependence of the data in Fig. (5) is clearly anomalous relative to $\Delta C_{p,\text{hyd}}$.

There are several potential explanations for the anomalous temperature dependence of the ΔH_{hyd} data in Fig. (5). One potential explanation is that this disparity is related to the decrease in hydration capacity with temperature noted above, with differences in the energetics of the unoccupied water sites from those filled during the experiments. If this were true, however, ΔH_{hyd} for the sites filled last would most likely be less exothermic than the first ones to fill, as observed in other zeolites [16, 23]. Furthermore, there is no indication of changes in ΔH_{hyd} as a function of hydration state in any of the results from the present study. A more likely explanation, which is consistent with the thermodynamic behavior discussed below, is that C_p is not a linear function of hydration state in the hydrated-dehydrated natrolite solid solution (in which case the disparity between the C_p and ΔH_{hyd} data would not exist), but rather that excess heat capacity of mixing (C_p^{EX}) is present in this solid solution. In this case, the difference between $\Delta C_{p,\text{hyd}}$ determined by regression of the data in Fig. (5) and that assessed from C_p for hydrated and dehydrated natrolite [~ 50 J/mol(H₂O)K] corresponds to the integral of C_p^{EX} over $X_{\text{hydrated natrolite}}$.

5. DISCUSSION: NATURE OF THE HYDRATED NATROLITE-DEHYDRATED NATROLITE SOLID SOLUTION

The hydration and dehydration behavior of natrolite is anomalous relative to that observed in other zeolites. Most zeolites exhibit fully reversible hydration/dehydration in which similar water contents are achieved under identical conditions of temperature, pressure, and the chemical potential of H₂O during both hydration and dehydration [e.g., 15, 16, 30] if sufficient time is afforded for equilibration. In dynamic TGA experiments, such as that shown in Fig. (1), water loss from these zeolites occurs gradually over a protracted range of temperature [e.g., 13], particularly at both the low and high temperature portions of the reaction. Additionally, in isothermal hydration experiments, the rate of hydration typically decays exponentially after the reaction begins [e.g., 15, 16, 23]. Natrolite, however, exhibits very different behaviors in these types of experiments, particularly at low

degrees of hydration. First, there is considerable hysteresis between water contents achieved during hydration and dehydration under the same conditions. For instance, water contents achieved during cooling of natrolite at constant $P_{\text{H}_2\text{O}}$ are considerably lower than those obtained during heating [13]. It is important to note that this hysteresis is not a kinetic effect, as it is repeatable and time-independent, and that it is most pronounced at low degrees of hydration [13]. Second, during dynamic TGA experiments the dehydration reaction proceeds at first gradually, as in other zeolites, and then goes to completion abruptly without a gradual mass loss at the end (high temperature portion) of the reaction (Fig. 1). Lastly, at relatively low degree of hydration, natrolite exhibits an unusual near zero-order rate of hydration (Figs. 2, 3, and 4). Thus there appear to be two distinct phenomena observed in the hydration and dehydration of natrolite: 1) at high degrees of hydration, natrolite exhibits behavior similar to reversible hydration observed in other zeolites; and 2) at relatively low degrees of hydration, natrolite exhibits an abrupt, stepwise hydration/dehydration behavior more akin to that found in hydrate minerals.

The best explanation for the hydration/dehydration behaviors observed in natrolite is that the solid solution between hydrated and dehydrated natrolite is characterized by an asymmetrical solvus that leads to immiscibility between dehydrated natrolite and natrolite exhibiting relatively high degrees of hydration. The abrupt/zero-order hydration/dehydration behavior noted at relatively low degrees of hydration is readily explained if continuous, reversible hydration is not possible due to immiscibility, leading to a step function change in hydration state as a function of time or intensive variables (e.g., temperature in Fig. (1)). It appears that the compositional extent of the solvus decreases with increasing temperature, as shown by the decreasing extent of the zero-order region in Fig. (4). At relatively low temperatures (e.g., Fig. 2) nearly complete immiscibility is present between hydrated and dehydrated natrolite, but with increasing temperature complete solution is possible between hydrated natrolite and an expanding range of hydration states.

If such a solvus exists, this may explain the anomalous temperature dependence of ΔH_{hyd} found in this study. Although not a necessary condition for the presence of a solvus, the presence of C_p^{EX} is a common condition in immiscible systems. An alternative explanation is that the excess enthalpy of mixing, H^{EX} , that gives rise to this solvus is contributing to the heat effects measured in our experiment. If this were true, the effect would arise from differential partial molar enthalpies of hydration between the miscible and immiscible portions of the solution. This behavior is not consistent with our observations which indicate that ΔH_{hyd} does not vary across the solution. Unfortunately, the partially hydrated members of this solution are not quenchable, precluding independent assessment of the magnitude of H^{EX} as a function of composition.

The solvus behavior noted above is probably present in a number of other confined water systems involving mineral hydrates. This is probably best established in the case of mesoporous materials, which exhibit hysteretic hydration/dehydration behavior similar to that found in natrolite that is now interpreted in terms of solvus behavior [e.g., 31]. Hysteretic behavior is also noted in the stepwise hydration of

smectite clay and in the hyperhydration reaction leading to fully-hydrated laumontite [32, 33]. In both of the latter cases, X-ray diffraction observations suggest that the compositional region exhibiting hysteretic behavior is characterized by the presence of two phases, as one would expect from the immiscibility proposed in the present work. The abrupt cessation of reaction noted in the dynamic TGA data for natrolite also appears to be typical of these solvus systems, as we have found both mesoporous materials and dehydration of the hyperhydrate form of laumontite to exhibit this behavior.

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