

Drill & Blast Workshop

L. Mirabelli and A. Lislrud



**QUARRY
ACADEMY**

Improving Processes. Instilling Expertise.

Balcones Quarry – 11.19.2014

| | |
|----------------------|------------------------------------|
| Rock type | Limestone |
| Bench height | 72 – 88 ft |
| Drill-hole | Ø6½" |
| Spacing | 19 ft |
| Burden | 25 ft |
| Bottom charge | 15 ft / 35%Emul-65%ANFO |
| Pipe charge | ~ 60 ft / ANFO |
| Subdrill | 5 ft |
| Uncharged | 10 ft |
| Stem material | ½" - ¾" |
| Rows | 1 |
| Hole delays | 39 ms / Digishot |
| Primers | Bottom 1 lb / Top ¾ lb |
| | Same delay top & bottom |



Safety of inpit operations

Tramming



Rollover from terrain bench – 115 ft drop

Fire in motor



Drilling into dynamite



Safety of inpit operations

- ***unwanted incidences do not just happen – they have root causes***
- ***actions can be taken so as to reduce frequency and consequences of unwanted occurrences***
- ***the relationship between complexity and knowledge in the workforce is often unbalanced - e.g. operator hazard training is a must!***



Premature ignition of electric detonators and blast due to lightning



Pit wall failure burying 3 drill rigs in rubble



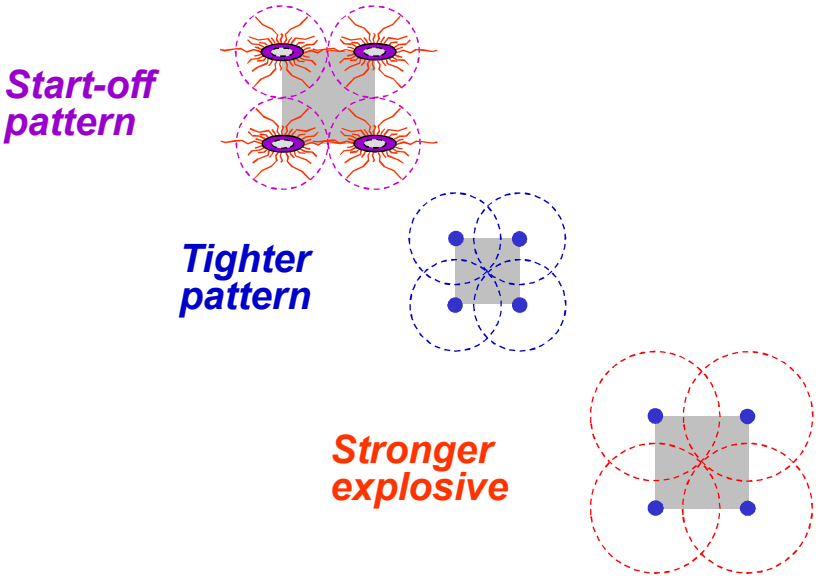
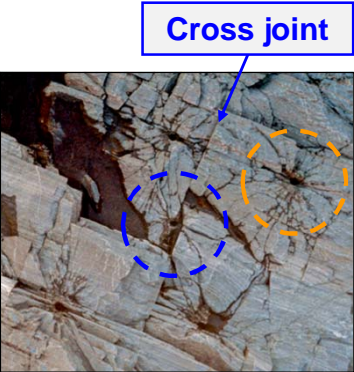
Some elements for successful blasting operations

- *match drill and blast patterns to rock conditions*
- *match shotrock fragmentation to worksite requirements*
- *match muckpile profiles to digger*
- *rate explosives performance by VOD measurements*
- *minimise blast damage in highwalls, control ground vibrations and flyrock*
- *straight hole drilling*

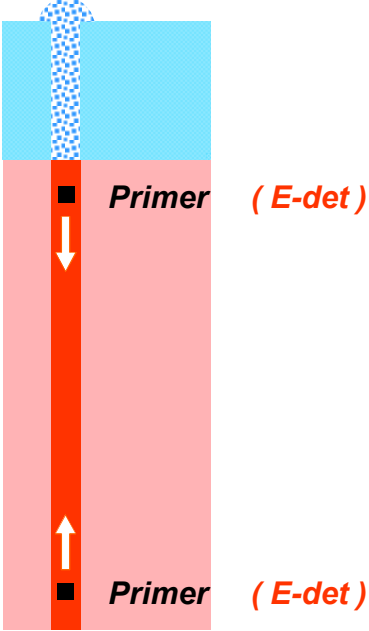


How finer fragmentation can be achieved

- enhance overlap of radial fractures from neighbouring blastholes
- enhance growth of radial fractures by stress wave re-enforcement



Stress wave timing

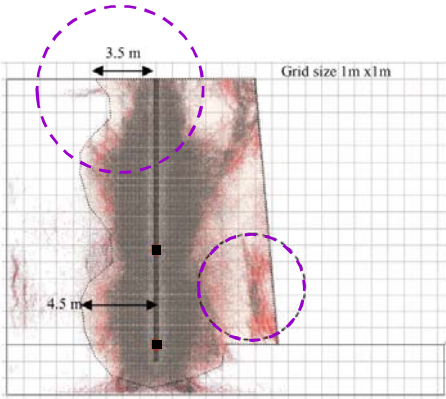
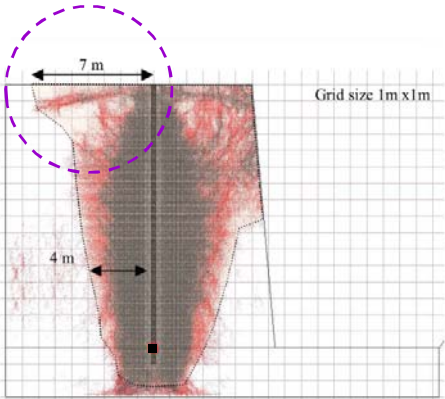
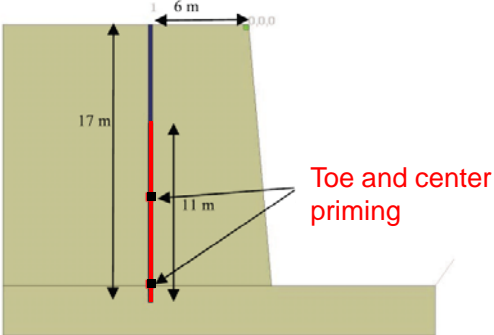
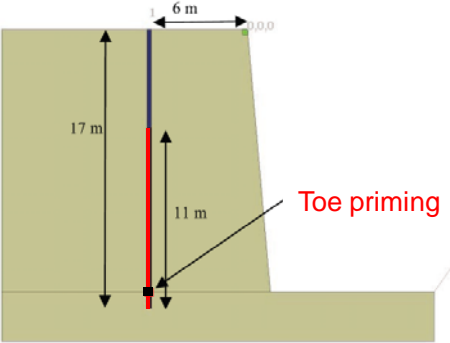


Example of blasting tighter drill patterns and use of E-dets

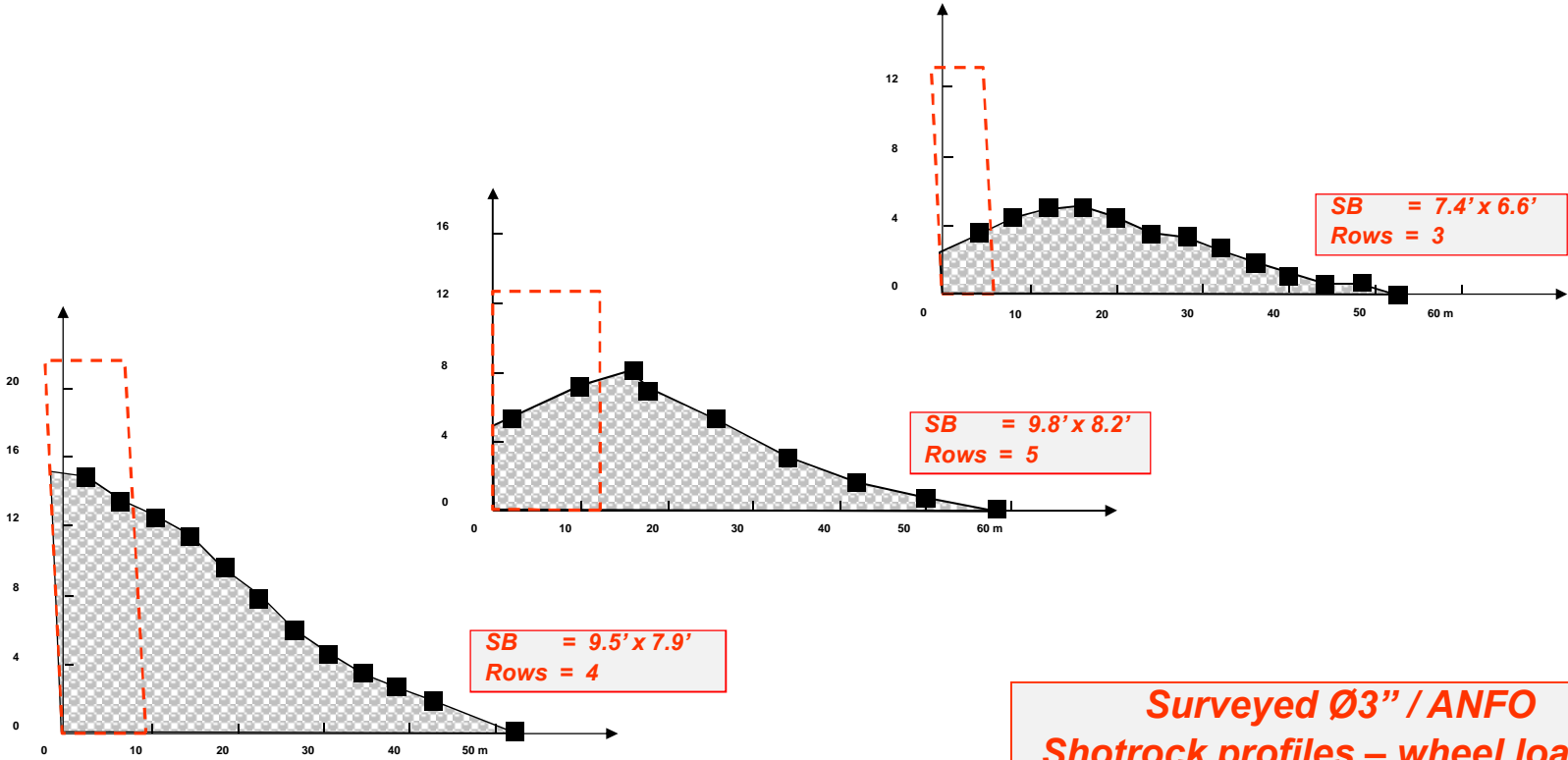


Blast damage reduction to crests

Example of HSBM modelling of a $\text{Ø}9\frac{1}{2}$ " emulsion charged blasthole with E-dets

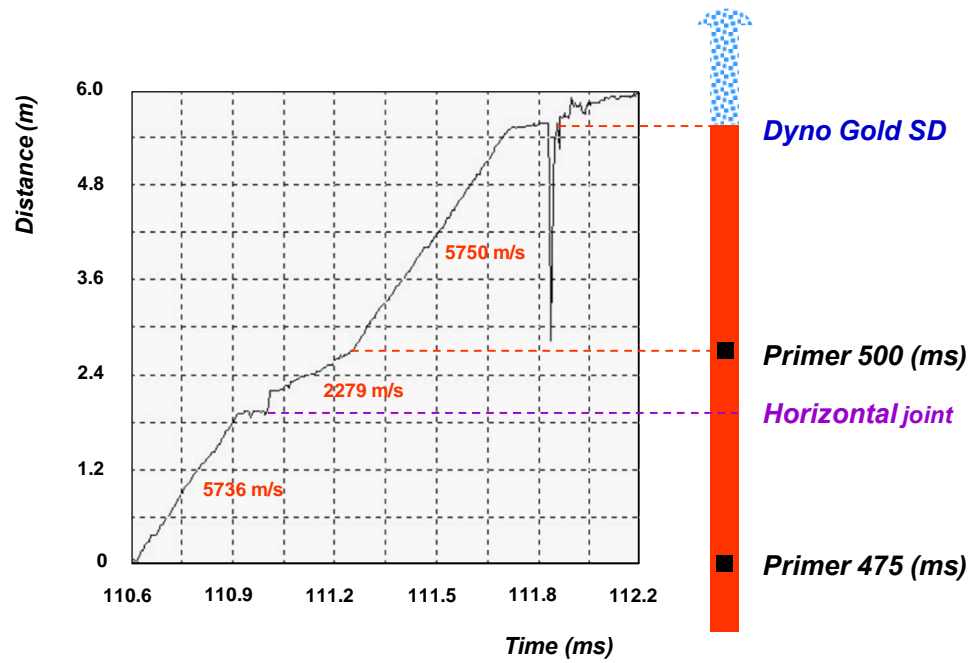
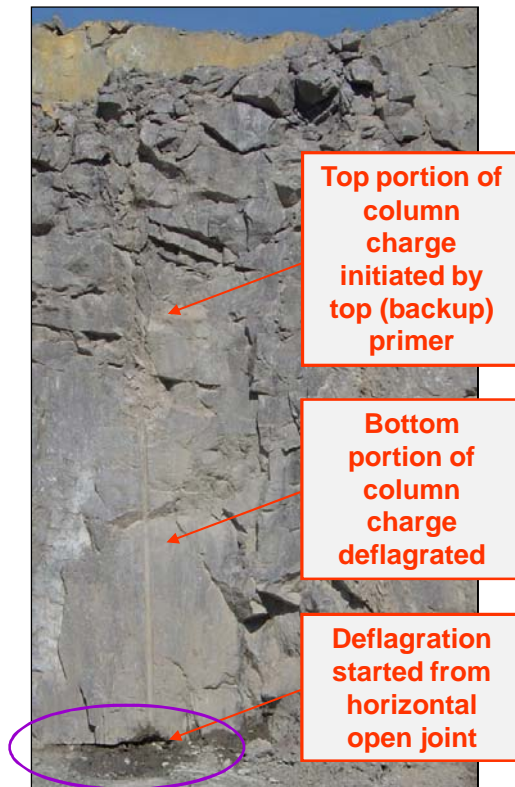


Shaping muckpiles to maximise dig rates



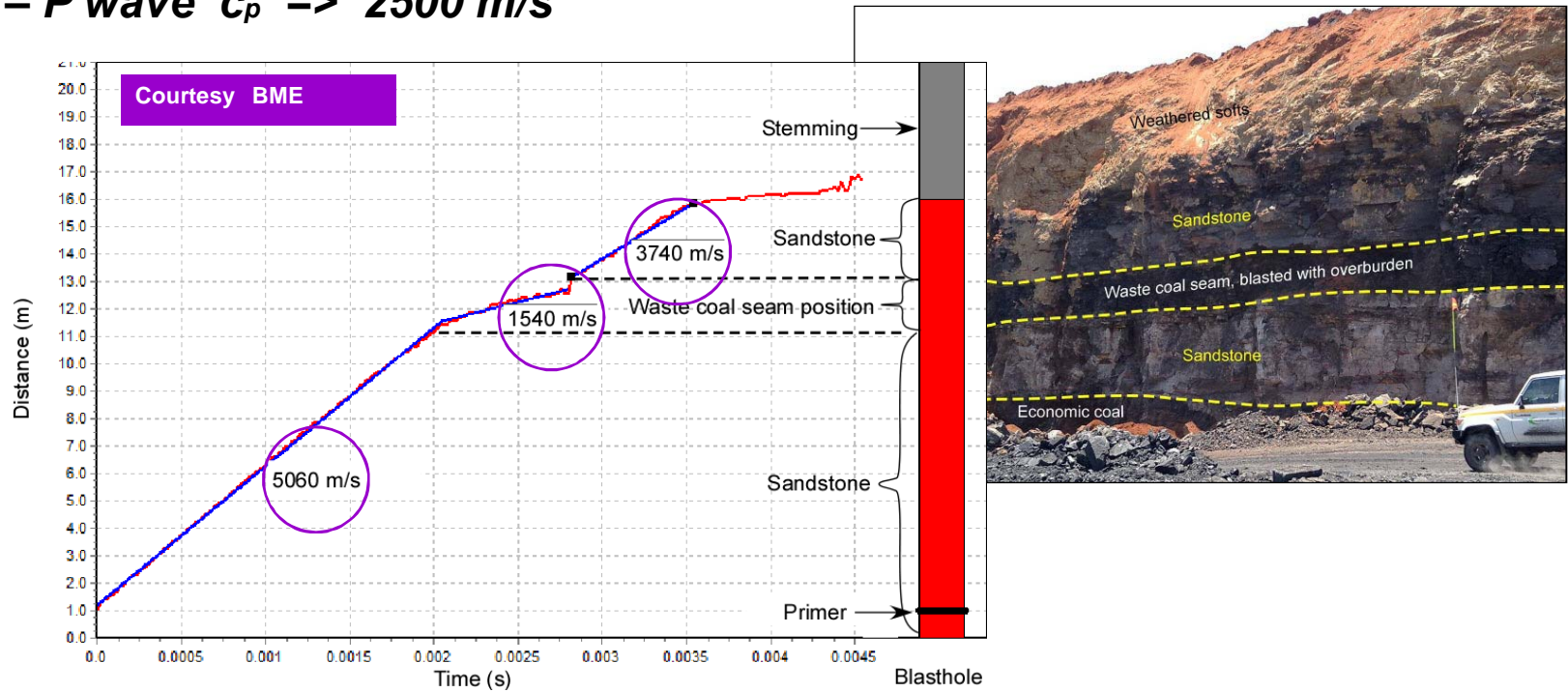
**Surveyed $\varnothing 3''$ / ANFO
Shotrock profiles – wheel loaders**

Explosives performance rated by VOD measurements



Explosives performance rated by VOD measurements

- $\text{Ø}9\frac{7}{8}"$ – gassed emulsion blend
- sandstone – P wave $c_p \Rightarrow 3900 \text{ m/s}$
- waste seam – P wave $c_p \Rightarrow 2500 \text{ m/s}$



Shocked loaded E-dets

- ***retrieved E-det from misfired blasthole internal electronic components damage by shock wave / pressure from adjacent blasthole***
- ***always consider time delay between adjacent blastholes and their effect on explosives or detonators***
- ***consider geology and water conditions in rock mass. Easy path for transmission of high shock / pressures.***
- ***select cast booster with shock resistant feature as best practice***
- ***brass sleeve within the detonator well. Protects the electronic components of the detonator.***

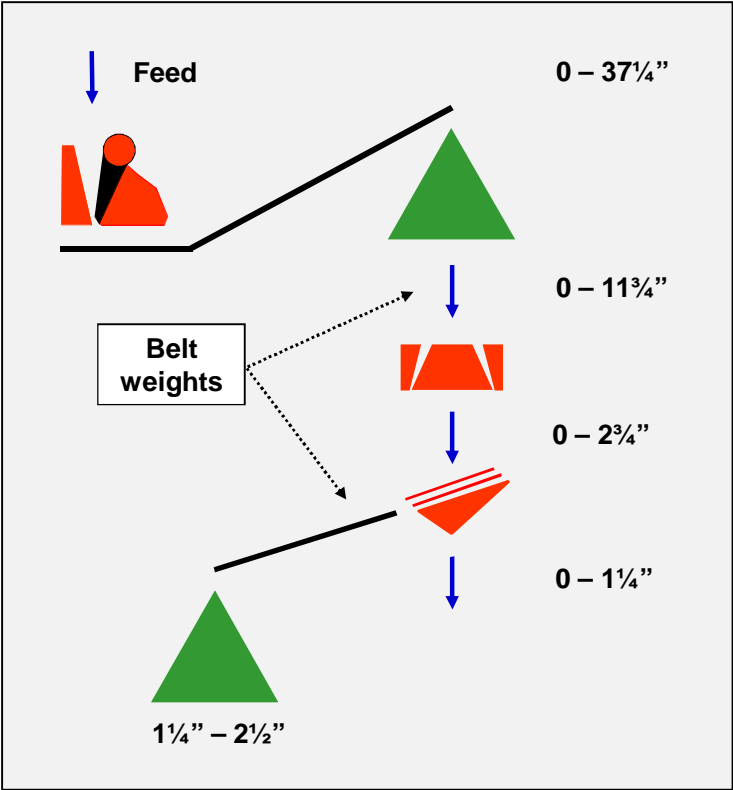
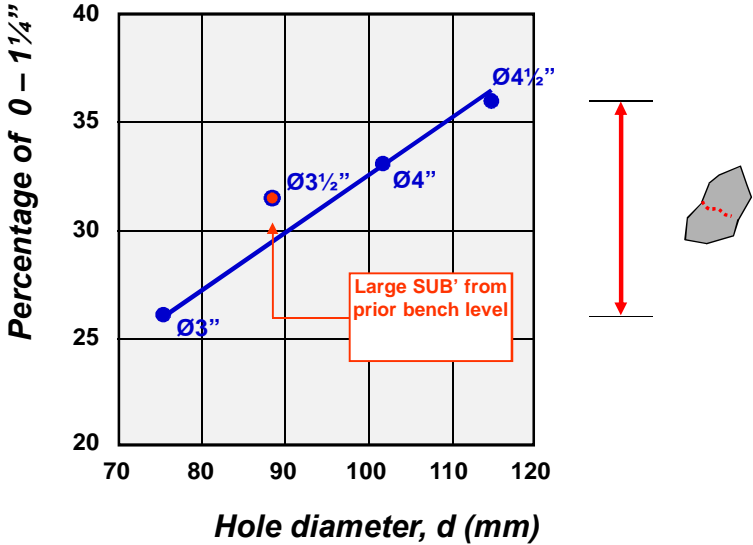


Some local site conditions

- **hole size (versus backbreak)**
 - ⇒ **charge concentration (lbs/ft)**
 - ⇒ **charge distribution (length of stem)**
- **terrain benches**
 - ⇒ **excessive amount of boulders**
- **shotrock fragmentation**
 - ⇒ **boulders, fines in shotrock and plant processing**
- **backbreak**
 - ⇒ **difficult 1st row drilling**
- **floor humps**
 - ⇒ **shotrock diggability**
- **drill-hole deviation**
 - ⇒ **floor humps, flyrock, broken steels, ...**
- **broken rock / open joints**
 - ⇒ **best with DTH**
- **blast vibrations**
 - ⇒ **record keeping, data analysis, neighbourly relations**

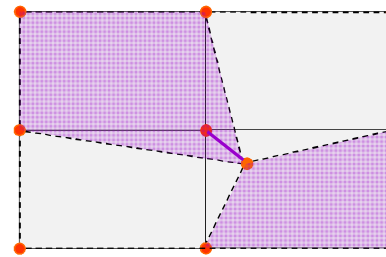
Quality plant feed – effect of fragment micro-fracturing

Rock type Anorthosite
Explosive Gassed emulsion
Test blasts 4 x 50,000 tons
Bench height 36'



What happens when we shoot holes that look like spaghetti?

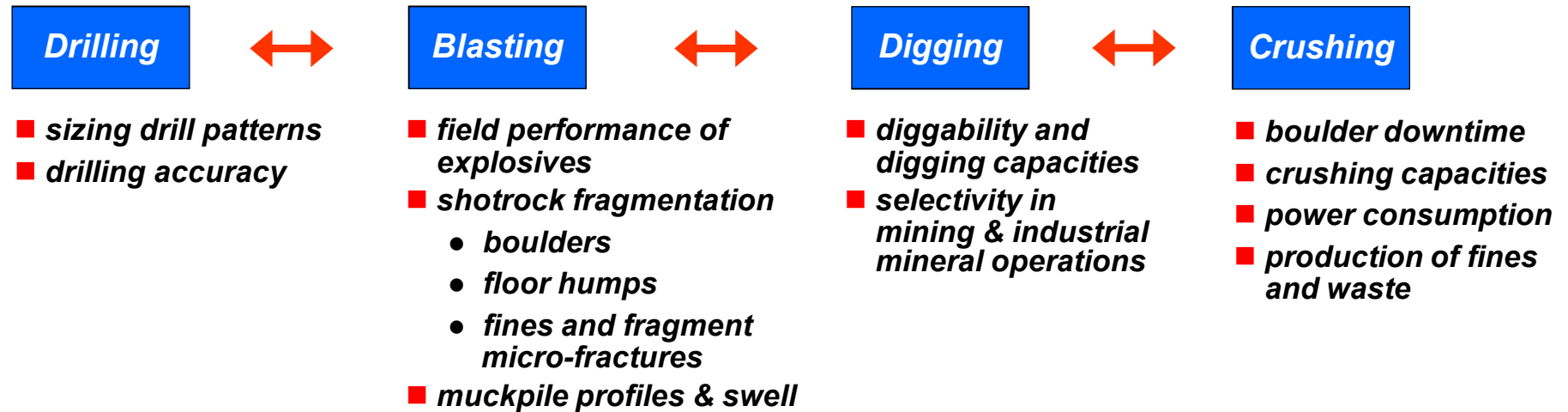
- ***blast patterns change locally (at hole bottoms)***
- ***floor humps***
- ***poor walls***
- ***flyrock from walls***
- ***blast direction***
- ***shothole deflagration / misfires***
- ***good practice***



- **Drill-hole collar positions**
- **Drill-hole positions at hole bottom**

- => ***poor loading conditions, uneven floors***
- => ***unstable walls***
- => ***difficult 1st row drilling and blasting***
- => ***safety, dust, toes, ...***
- => ***quality of floors and walls***
- => ***safety / explosives in muckpile***
- => ***locally choked muckpiles (poor diggability)***
- => ***max. drill-hole deviation up to 2 – 3% for production drilling***

How D&B affect down-stream operations

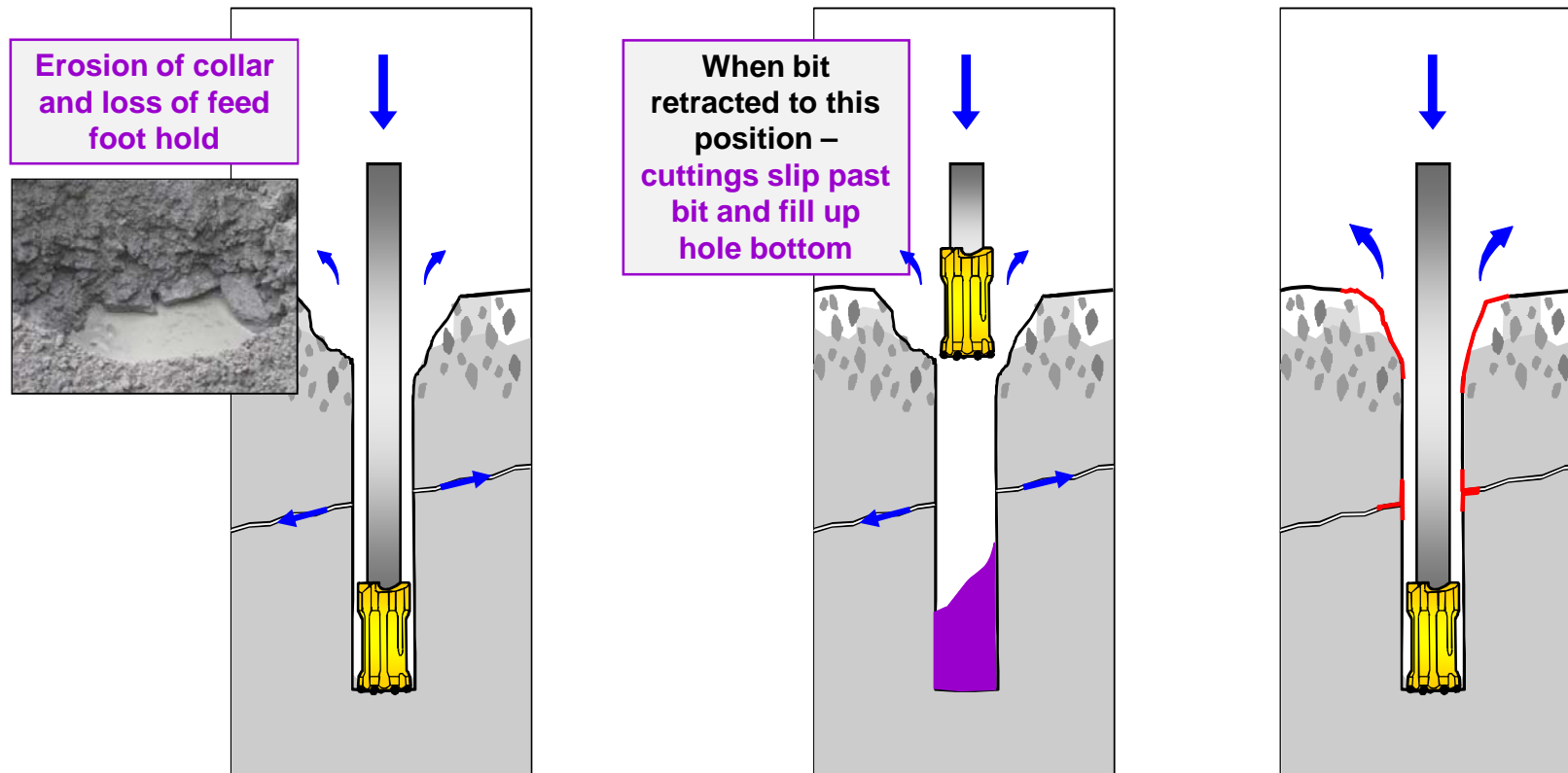


Some typical problems in drilling operations

- ***flushing / cuttings removal / collapsing holes***
- ***over-worn bits***
- ***pressure settings / low drill steel service life***
- ***drill-hole deviation***
- ***difficult 1st row drilling***



Foams seal and stabilise walls - and improve flushing



Over-worn bits – what to do?



Gauge buttons heavily worn down due to too high bit RPM's (i.e. adhesive wear)

$$V_{gauge} = \pi \cdot 4/12 / (60 / 122) \\ = 1.6 \text{ ft/s}$$

Broken buttons due to snakeskin – regrind more so as to remove the snakeskin layer !

Limestone **2.3 ft/s**

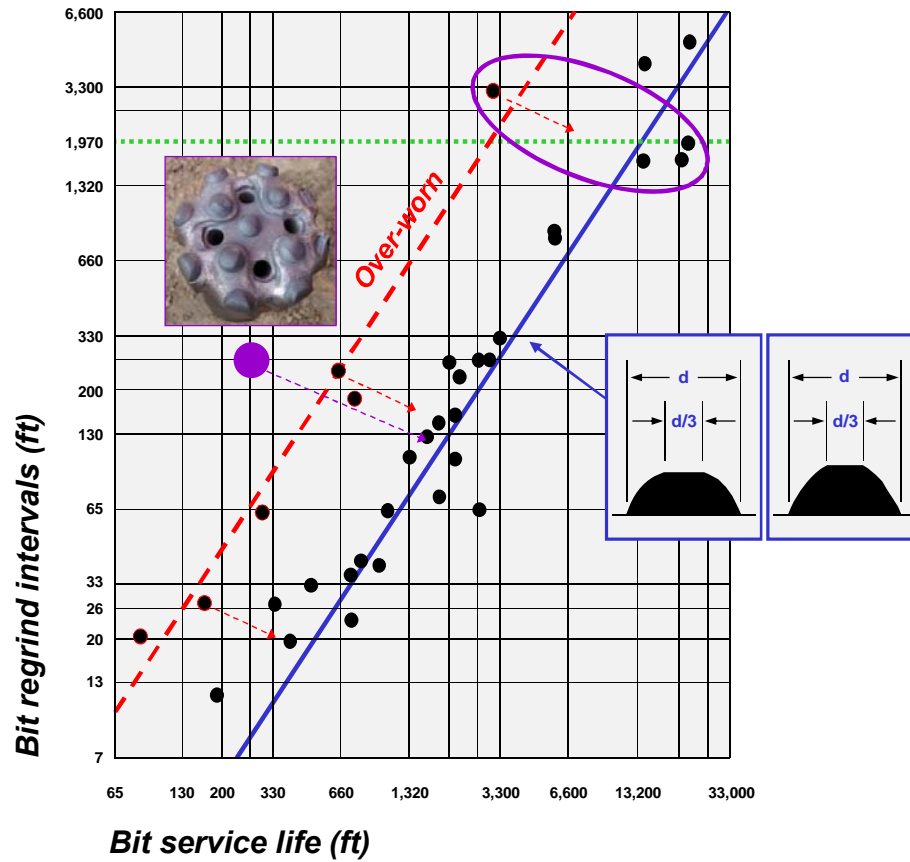
Granite **1.3 ft/s**

Quartzite **0.8 ft/s**

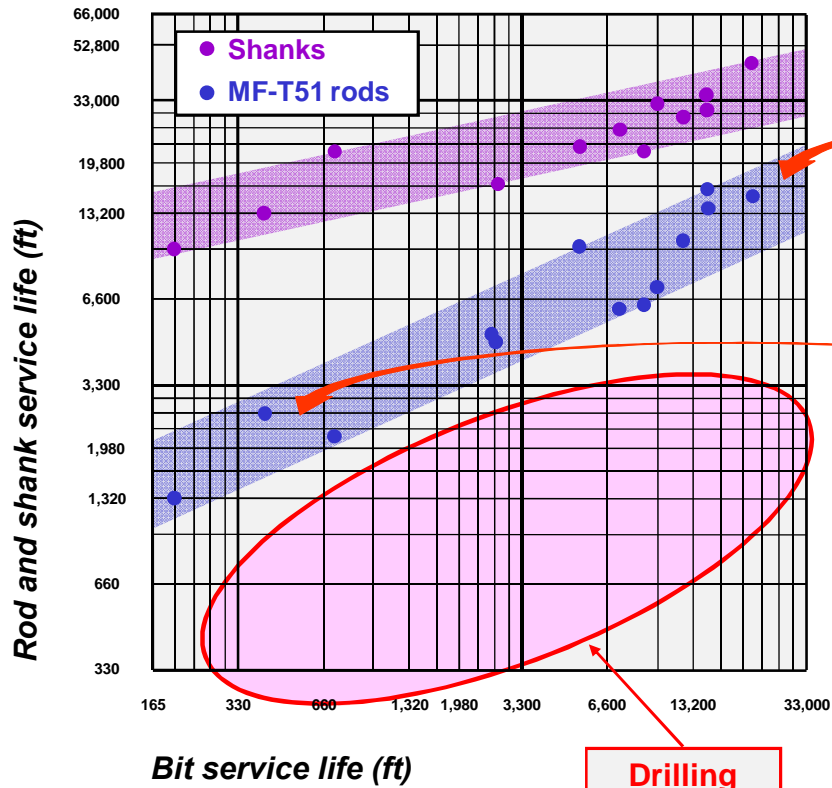
Bit regrind intervals, bit service life and over-worn bits



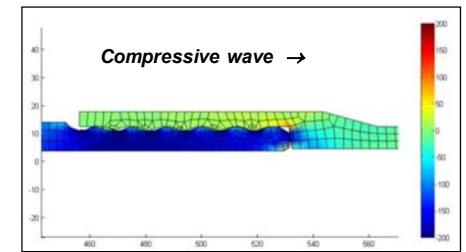
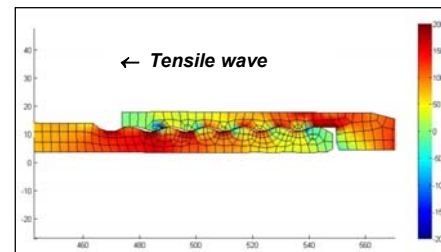
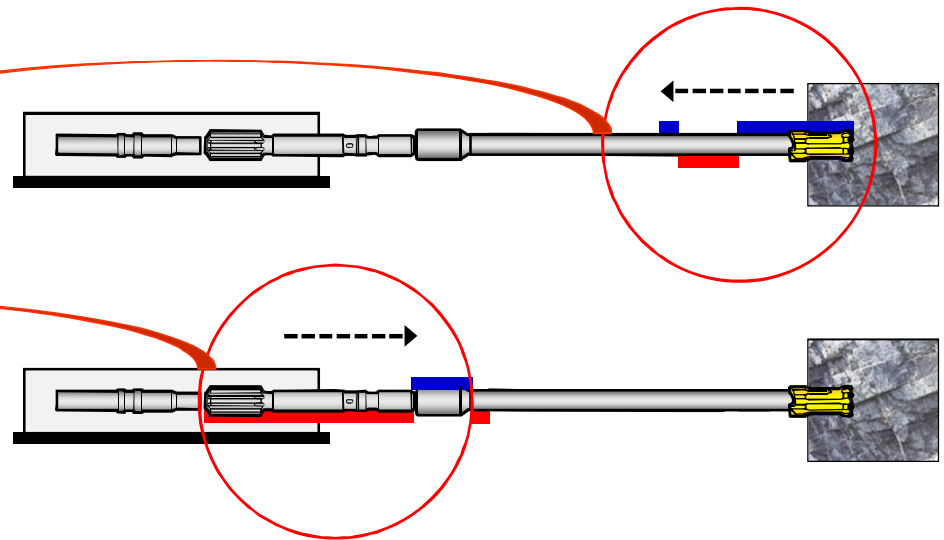
Premature
button
failures



Tensile waves reduce drill steel service life

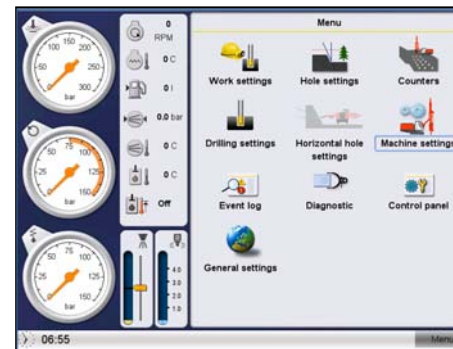


Drilling with underfeed



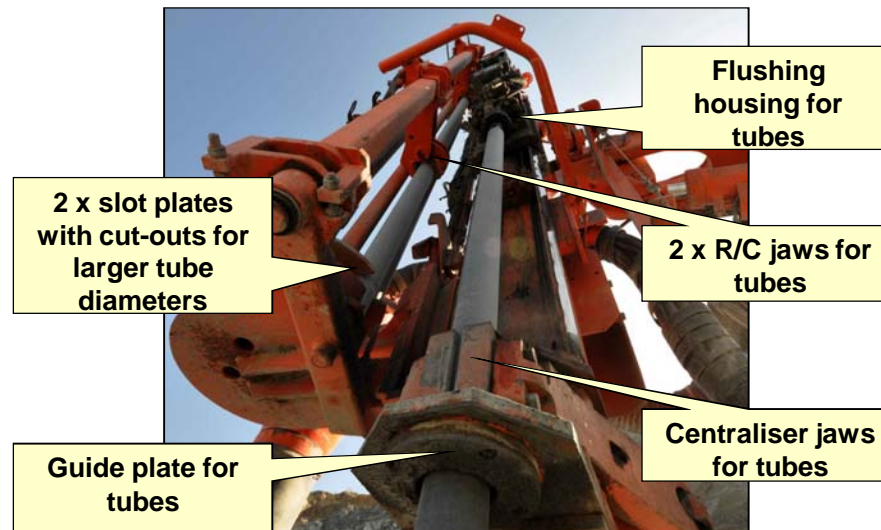
What drilling controls do

- **feed speed control** ⇒ **avoid bit rushing through joints and voids**
- **anti-jamming** ⇒ **avoid stuck drill steel and rod breakage**
⇒ **frequently activated – a sign of poor flushing?**
⇒ **frequently activated - results in STOP-GO drilling due to recollaring algorithm**
- **percussion-feed linkup** ⇒ **avoids under and over feeding**
- **torque control** ⇒ **smooth drilling through joints, avoids STOP-GO, ...**
- **no system for bit selection ...**



TH Tube drilling – avoid:

- **bending of drill string** - *leads to premature tube failures*
- **heavy rebounds** or **bit service life < 5700 ft** - *leads to poor tube life*
- **jerky tube rotation** - *leads to an unstable bit which initiates drill-hole deviation*

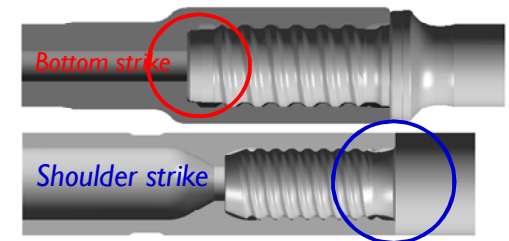


Case study - Singrauli Mine

- **Rock** **Overburden sandstone**
- **Drill rig** **P1524 / HL1560 / chain feed**
- **Tubes** **ST68 threads / Ø96mm / 2 x 12' SP**
- **Bits** **6" Retracs**

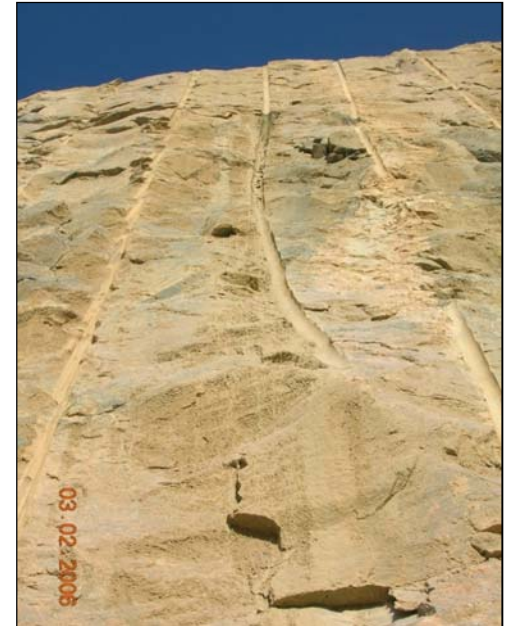
- **Bit penetration rate** **367 ft/ph = 6.13 ft/min**
- **Feed ratio** **90 bar / 150 bar = 0.60**

- **bit service life** **18,620'**
- **shank service life** **11,770' / 62,745' / 84,720'**
- **tube service life** **4,465' / 16,585' / 36,680'**



How do we go about drilling straighter holes?

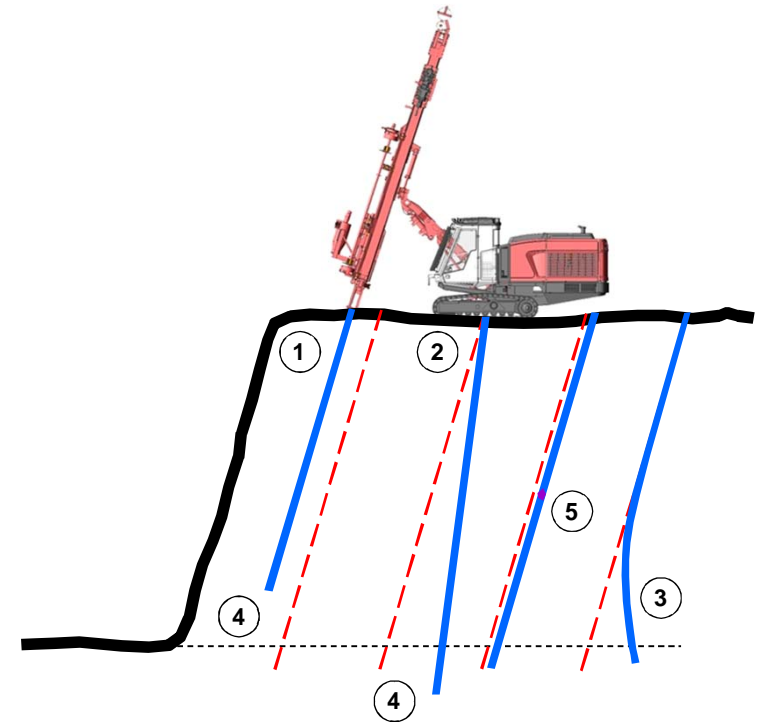
- *understand the many issues leading to drill-hole deviation*
- *technically good drill string*
- *technically good drill rig, instrumentation, ...*
- *motivate the drillers!*



Accurate drilling gives effective blasting

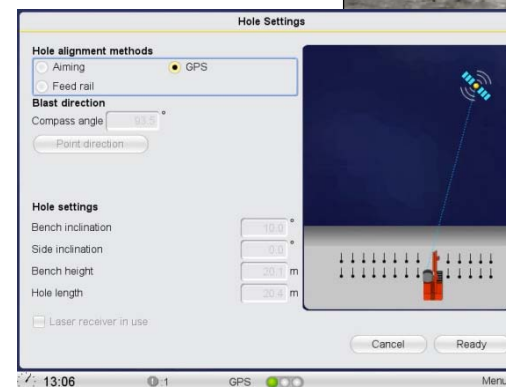
Sources of drilling error

1. **Collar position**
2. **Hole inclination and direction**
3. **Deflection (bending)**
4. **Hole depth**
5. **Omitted or lost holes**
6. **Shothole diameter (worn out bits)**



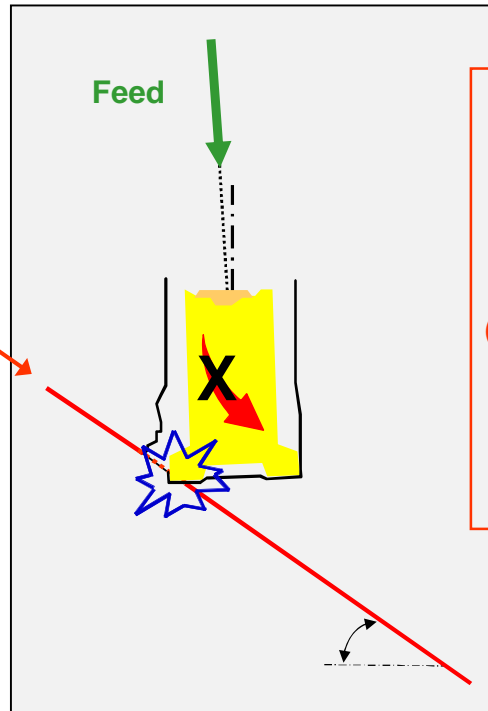
Collar position error control

- **use tape, optical squares or alignment lasers for measuring in collar positions**
- **use GPS or total stations to measure in collar positions**
- **collar positions should be marked using painted lines – not movable objects such as rocks etc.**
- **completed drillholes should be protected by shothole plugs etc. to prevent holes from caving in (and filling up)**
- **use GPS guided rig mounted collar positioning devices e.g. TIM-3D**



Difficult 1st row drilling:
- avoid flyrock
- avoid floor humps

How bit face designs enhance drill-hole straightness

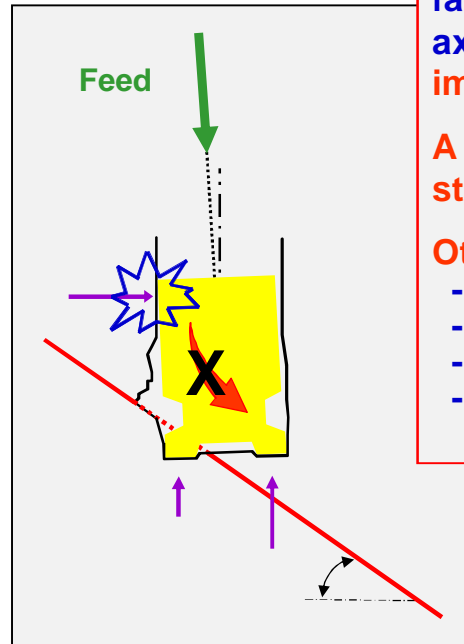


When the bit first starts to penetrate through the joint surface on the hole bottom - the gauge buttons tend to skid off this surface and thus deflect the bit.

More aggressively shaped gauge inserts (ballistic / chisel inserts) and bit face gauge profiles (drop center) reduce this skidding effect by enabling the gauge buttons to “cut” through the joint surface quickly - thus resulting in less overall bit deflection.



How bit skirt designs enhance drill-hole straightness



As the bit cuts through the joint surface - an uneven bit face loading condition arises; resulting in bit and drill string axial rotation - which is proportional to bit impact force imbalance.

A rear bit skirt support (retrac type bits) reduces bit and string axial rotation by “centralizing” the bit.

Other counter measures:

- longer bit body
- add pilot tube behind bit
- lower impact energy
- rapid drilling control system reacting to varying torque and feed conditions



Some strength and weaknesses

| | <i>TH</i> | <i>DTH</i> | <i>Rotary</i> |
|---------------------------------|-------------------------------------|---------------------|---------------------|
| ■ <i>General weaknesses</i> | - drill string - operator skills | - fuel efficiency | - heavy rig |
| ■ <i>Drill steel</i> | - rods / tubes | - tubes | - tubes |
| ■ <i>Soft rock</i> | good | good + | good + |
| ■ <i>Hard rock</i> | good + | good - (rot. heads) | good (for big bits) |
| ■ <i>Broken rock (flushing)</i> | good - | good | good - |
| ■ <i>Running water</i> | OK | OK - | OK - |
| ■ <i>High altitude</i> | | | |

Lafarge Bath Operations, Ontario

Annual production **1.6 mill. tons**
Rock type **Limestone**

| | |
|--------------------------------|------------------------------------------------|
| Bench height | 105' |
| Bit | Ø115mm - 4½" guide XDC |
| Drill steel | Sandvik 60 + pilot tube |
| Hole-bottom deflection | < 1.5 % |
| Gross drilling capacity | 220 ft/hr |
| Drill pattern | 14¾' x 15¾' (staggered) |
| Sub-drill | 0' (blast to fault line) |
| Stemming | 9¼' |
| No. of decks | 3 |
| Stem between decks | 5.9' |
| Deck delays | 25 milliseconds |
| Charge per shothole | 520 lbs |
| Explosives | ANFO (0.95 & 0.85 g/cm³) |
| Powder factor | 0.57 lb/yd³ |



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